

818 S. FLORES ST.

attached.

SAN ANTONIO, TEXAS 78204

www.saha.org

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Procurement Department

ADDENDUM # 2

To: File 1911-913-45-4982 <u>RFP for: Pecan Hill Tree Removal and Sanitary Sewer Retrofit</u> *Please note the following changes:*

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- 1. The response due date and time are changed to January 31, 2020 at 2:00 pm.
- 2. Questions may be submitted until 2:00 pm on January 17, 2020.

The following questions are asked:

Question 1: Answer 1:	What is the engineered budget? SAHA estimates the construction costs to fall within the \$400,000 to \$650,000 range.
Question 2:	What effort has been put into locating the existing sewer line under the slab? Has a plumber used a camera to locate the lines and risers? If so, is there a report we can see?
Answer 2:	The main lines have been scoped with a plumbing camera. The report is attached.
Question 3:	If not, Will it be expected of us to locate the lines prior to excavation? If there are additional locations that aren't shown on the drawings that require additional work what would be the expectation of the contractor and owner?
Answer 3:	See above answer.
Question 4:	Units 115-120 do not show to be re-piped. Please provide clarification as to why we would abandon these lines.
Answer 4:	Units 115 – 120 should be re-piped according to Drawing P1.1 and tied into the existing sewer line on the south side of the complex.
Question 5: Answer 5:	What is the expectation to route the sewer line near electrical pole? Please refer to Drawing P1.0, Detail 5, Pipe Trench Detail. The sewer line should be routed a minimum distance of 2x the pole diameter away from the base of the pole.
Question 6: Answer 6:	Is there a GeoTech report available for review? We have a limited Geotechnical report that was performed in 2016. The boring logs are



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Question 7:	Will the cost of concrete chipping for exposing fittings etcfor sanitary sewer lines be addressed on a case by case scenario in order to replace sewer lines and make successful connections.
Answer 7:	Concrete chipping should be included as a Unit Cost Item; although concrete chipping is not expected.
Question 8: Answer 8:	Can we submit latest Tax Return in Lieu of Financial Statements? Yes they are acceptable. All we need to do is verify the financial health of the company and that it has the capacity to accept a contract of this size without undue stress.
Question 9: Answer 9:	Is there any As-Builts showing the foundation beam depths, thickness and lay-out? We have the original construction drawings. See attached.
Question 10: Answer 10:	Do you have As-Builts showing Depth of Sewer Piping under foundation and type of existing piping? We have the original construction drawings. See attached.
Question 11: Answer 11:	Are there As-Builts that show existing utilities in new excavation area, Electrical, Cable, Gas? We have the original construction drawings. See attached.
Question 12: Answer 12:	Drawings show 2 pipe handrail system BUT Specs descripts Stainless Steel, Painted Steel, aluminum, which is required for this project? Handrail is a basis of design product that must meet the minimum specifications. Final decision for finish will be made by the Owner.
Question 13: Answer 13:	Can Schedule 40 piping be used for the repairs of this project? PVC pipe should be in compliance with ASTM listed in Specification section 221313.
Question 14: Answer 14:	If we need to can we Core Thru the existing concrete building beans to maintain the proper fall/flow of piping? Coring through the middle third of the beam depth will be allowed with Engineer's approval.
Question 15: Answer 15:	Can more days be negotiated for completion of project? If the Respondent feels the days shown are inadequate they may indicate the days they feel that will be needed on the Fee Sheet.
Question 16: Answer 16:	Are there any Soil Test reports to tell us if rock or hard soil will be encountered while digging? See answer 6.
Question 17: Answer 17:	Manhole depth on page P1.2 , is the Manhole depth in Inches or Feet? Inches. However, manhole depth should be field verified.
Question 18:	If a road closure is required, can we close one side of the building for trenching at a time for dirt removal etc.?

Answer 18: This would need to be coordinated with the Project Manager and the Property Manager.



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Question 19: Can the work schedule include longer day hours and include week-end hours later then 8 to 5?Answer 19: Weekdays SAHA may allow for a 7am to 6pm schedule, weekends will be on a as needed or case by case basis.

Question 20: Can we please have the Magnitude of this project? This is needed for insurance purposes. **Answer 20:** See Answer 1.

The Jan 10, 2020 site visit sign in sheets are attached.

By: Charles RBode

Date: January 13, 2020

Charles Bode Asst. Director of Procurement

Marvin E Williams Paul Scott Jr Jorge A Zapata Jorge A Zapata Jorge A Zapata Jorge A Zapata Jorge A Zapata Jorge A Zapata Jorge A Laker Jean Carter Jean Carter	REPRESENTATIVE NAME
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Project No. ASR16-034-00 December 19, 2016



Raba Kistner Consultants, Inc. 12821 W. Golden Lane San Antonio, TX 78249 P.O. Box 690287 San Antonio, TX 78269 www.rkci.com

> P 210 :: 699 :: 9090 F 210 :: 699 :: 6426 TBPE Firm F-3257

Mr. Marvin Williams, Construction Project Manager San Antonio Housing Authority 818 S. Flores San Antonio, Texas 78204

RE: Foundation Movement Study Pecan Hill Apartments 1600 West Lawndale San Antonio, Texas

Dear Mr. Williams:

RABA KISTNER Consultants, Inc. (RKCI) is pleased to submit our report of engineering services for the above referenced project. This document describes the services that RKCI has performed in accordance with the scope of work outlined in our Proposal Number PSR16-062-00 (Revised) dated July 29, 2016. We were retained to provide engineering consulting services in an effort to identify the causation of foundation movement and to provide recommendations for repairs.

In summary, the apartment complex situated at 1600 West Lawndale has experienced differential movements that are affecting the performance of the floor slab, interior partition walls and ceilings, exterior walkways, underground plumbing, facade treatments and the roofing systems. These conditions of deterioration range from mild to severe and are widespread throughout the apartment complex. Although remedial foundation repairs are not recommended at this time, other building systems require immediate attention.

We appreciate the opportunity to be of service to you on this project. Should you have any questions about the information presented in this report, or if we may be of additional assistance, please call.

Very truly yours,

RABA KISTNER CONSULTANTS, INC.

Robert L. Raffle, P.E., S.E., M.E., AIA, NCARB Senior Forensic Architect/Engineer

RLR/ESR/jg

Attachments

Copies Submitted: Above (Via Email)

Eric S. Rypple, P.E. Manager, Forensic Services

FOUNDATION MOVEMENT STUDY

For

PECAN HILL APARTMENTS 1600 WEST LAWNDALE SAN ANTONIO, TEXAS

Prepared for

SAN ANTONIO HOUSING AUTHORITY

San Antonio, Texas

Prepared by

RABA KISTNER CONSULTANTS, INC. San Antonio, Texas

PROJECT NO. ASR16-034-00

December 19, 2016

RABAKISTNER

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1.0 INTRODUCTION

Raba Kistner Consultants, Inc. (RKCI) was commissioned by the San Antonio Housing Authority (Client) to perform a Foundation Movement Study at Pecan Hill Apartments situated at 1600 West Lawndale in San Antonio, Texas. The purpose for this study was to assess the type and causations of cracks, separations, and sloping floor slab conditions that developed within the apartment complex buildings as well as present our findings with opinions for our Client's consideration in determining the next course of action. As part of this work, RKCI conducted an interior floor elevation survey of the ground level of all buildings in addition to non-destructive testing, plumbing leak testing, exploratory borings on the exterior and interior, test pit excavations with subsequent laboratory testing of soil samples.

This report presents the findings of our assessment conducted over the course of several months in six sections including the Introduction. Section 2 - Background Information briefly discusses the general characteristics of the facility. Section 3 - Field Study presents the visual Ground Level and Roof Assessments. Section 4 - Benchmark Installation provides a detailed explanation of that process. Section 5 - Relative Floor Elevation Surveys and Contours quantifies and interprets that data. Section 6 - Plumbing leak Testing presents the results of camera observations. Section 7 - Borings and Laboratory Tests provide an in-depth look at the site geological and soil conditions along with the results of inhouse tests. Section 8 - Test Pit Observations identifies those findings. The culmination of this report is presented in Section 9 - Conclusions and Recommendations. Section 10 - Limitations outlines the limitations of this report. Attachments provides the field data collected and prepared including Appendix A – Photo Exhibits, Appendix B - Drawing Exhibits and Appendix C - Plumbing Leak Test Report.

2.0 BACKGROUND INFORMATION

Refer to Figure 1 for an aerial view of the apartment complex along with identifiers for each building based upon geographic orientation.



Figure 1: Aerial View of Pecan Hill Apartments (Looking North)

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Copies of the original construction documents were provided to RKCI via Dropbox on July 22, 2016. These documents included:

- Drawings 1 thru 34 prepared by Ralph C. Bender & Assoc. Inc. of San Antonio, TX, dated 3-21-78 with their consultants as follows:
 - Civil/Structural Maverick Engineering Company of Corpus Christi, TX (Dwgs. 1, 3-4, 6-8)
 - Mechanical/Electrical/Plumbing Anderson Engineering Company of San Antonio, TX (Dwgs. 24-34)
- Drawings 1 and 2 prepared by Ralph C. Bender & Assocs. Inc. of San Antonio, TX, dated 4-24-78.
- Drawings 1 and 2 prepared by Ralph C. Bender & Assocs. Inc. of San Antonio, TX, dated 6-7-78.

The apartment complex, built circa 1978, consists of four, three-story apartment buildings and a community center totaling approximately 24,700 sq.ft. According to the original structural drawings prepared by Maverick Engineering Company, the foundations are constructed of a post-tension slab-ongrade with interior and exterior grade beams. The beams are approximately 10-inches wide and range between 18 to 30-inches in depth. Some beams are founded on a total of ninety-one (91) 12-inch diameter shallow piers that extend 3-feet into the native soils and positioned predominantly on the south end of the East Building, throughout the South and West Buildings, the southern half of the Community Building and the outside corners of all four courtyard stairs. Eighty-seven (87) additional steel piers were installed throughout the complex in 1989 in accordance with direction provided by Cutler-Gallaway Services, Inc. of San Antonio, TX as part of a modernization project to stabilize and correct foundation/slab distress conditions prevalent at that time.

The Client also provided a copy of a Condition Study prepared by Accutech Consultants, LLC of San Antonio, TX for Vickery and Associates also of San Antonio, TX, dated August, 2011. This report confirms that remedial foundation work was conducted in 1989 by Cutler-Gallaway Services, Inc. Those drawings were not available but Appendix D contains an excerpt (Drawing 4) from Accutech's Condition Study that superimposes the original concrete foundation piers and the steel piers installed in 1989 which work included:

- Installation of eighty-seven (87) steel piers
 - Along the north, east and west exterior perimeters of the North Building.
 - Along the east exterior perimeter of the East Building.
 - Along the south exterior perimeter of the South Building.
 - Along the interior and north, west and south exterior perimeters of the West Building.
- Leveling of the foundations and grouting of void spaces.
- Epoxy injection of slab cracks.
- Grinding at construction joints to provide a smooth transition.

Accutech Consultants, LLC conducted an elevation survey of the first floor level which is included in this report in Appendix D, Drawing 4.

Accutech's recommendations in 2011 were:

- "Test the plumbing system to determine if there are any leaks beneath the foundation. ..."
- "Test the drain system in the courtyard to ensure it is functioning properly."
- "Regrade the area along the north side of the complex to direct water quickly away from the buildings. ..."
- "Install "root barrier" along the north and east side of the complex and along the south side of the [North Building] to prevent the tree roots from going beneath the foundation..."

- "Implement a water maintenance program. ..."
- "Once the above recommendations have been implemented, we recommend that a monitoring program be implemented to evaluate the effectiveness of the recommendations. This program generally consists of elevation surveys of each building on a three month interval. ..."

3.0 FIELD STUDY

A. GROUND LEVEL ASSESSMENTS

Observations of the interior and exterior of the apartment complex were performed on several dates by Mr. Eric Rypple, P.E. and Mr. Robert Raffle, P.E. of RKCI. Reference is made to Appendix A - Photo Exhibits, Photos 1 through 71 and Appendix B - Drawing Exhibits, Drawing C 1.2 - Photo Key Plans.

Cracking and material deterioration were observed throughout the complex including:

- Interior cracking of drywall partitions and ceilings.
- Interior cracking near cased and framed openings.
- Interior heaving of the floor slab primarily in kitchen areas.
- Rippling of the ceiling/wall joints.
- Interior cracking of vinyl tile.
- Noticeable sloping of interior slabs.
- Exterior cracking of concrete walkways and canopy soffits.
- Exterior cracking around framed openings.
- Deterioration of stucco facades including joint displacement and separation from substrate construction.
- Deterioration of building expansion joints.
- Exterior cracking of the facade.
- Isolated cracking of perimeter building foundations.
- Deterioration of pavement joints.

It should be noted that much of the distress listed above has been patched or previously repaired.

Environmental conditions that are contributing to building distress include:

- Improper drainage along the north and west buildings.
- Downspouts empty into the planter beds or in close proximity to the building foundations.
- Downspouts serving the West Building roof slope upwards instead of a positive downward slope.
- Large trees in close proximity to the building foundations especially in the courtyard areas around the Community Building and on the North side of the North Building. In some cases, root systems are visibly protruding and appear to extend under the buildings.

B. ROOF ASSESSMENT

On November 4, 2016, Mr. Albert White, Senior Building Envelope Consultant along with Mr. Weston Tietze, E.I.T. Technician performed a visual roof assessment. Generally, the roof consists of composition shingles with isolated areas, such as the central portion of the Community Building, using a relatively flat composition system.

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The existing shingled roofs are sloped at a rate of approximately 1/8" per foot on the low sloped granule surfaced asphalt roofs and between 4" and 8" per foot for the steep asphalt shingle roofs. The slope appears to have been provided by the roof's structural supports. The roofs were generally well drained although their condition ranges from poor to fair. Reference is made to Appendix A - Photo Exhibits, Photos 72 through 97 and Appendix B - Drawing Exhibits, Drawing C 1.2 - Photo Key Plans.

Numerous surface deficiencies were observed that included:

- Past repairs made with different colored asphalt shingles than the existing shingles.
- Roof to wall metal flashing missing or poorly installed and secured.
- Eave fascia boards separating from the substrate.
- Roofing material separation.
- Roof expansion joints covered with asphalt shingles.
- Vent pipe flashings are damaged or splitting.
- Rusted metal housings on roof-mounted vents.
- Leak paths into the building at stucco walls, metal flashing and eave fascia boards.
- Vent flashing damaged, unsecured or poorly secured.
- Head wall flashing is loose and damaged in several locations at stucco walls.
- Numerous soft spots in the decking from possible roof expansion joint deficiencies and water migration.
- Sealants are deteriorated and in generally poor condition.
- Roof to wall base flashing is poorly attached at the asphalt shingle roofs and could allow water migration to the interior framing especially under wind driven rain conditions.
- Hail damage from recent and past events.
- Moderate to severe deterioration of building and roof expansion joints.

4.0 BENCHMARK INSTALLATION

A permanent benchmark was installed on the south side of the property to facilitate monitoring of differential floor elevations. (Refer to Appendix B, Drawing C 1.0) A hole was bored to a depth of 30 feet and the 4-1/2 inch diameter borehole was cleaned out down to the rumination depth with straight flight augers. Sections of 2 inch diameter PVC were joined together to form a center casing between the borehole wall and the aluminum rod that is embedded into the soils at the bottom of the borehole. The aluminum rod was constructed of three, 10 foot long sections screwed together at the bottom of the hole. The outside annulus between the borehole wall and the outside of the PVC pipe was filled to a depth of about 18 inches below the top of the ground surface with a sand mixture.

A 12 inch thick layer of concrete was placed over the top of the sand to form an impermeable cap over the sand annulus. The area over the top of the benchmark location was excavated and formed to approximately 20 inches square and to a depth of approximately 4 inches below the top of the ground. An approximately 6 inch long, 4 inch diameter piece of PVC pipe, with a threaded cap, was connected to the top of the 2 inch diameter pipe to facilitate the installation of the survey pin. The excavation area was then filled with ready-mix concrete that was trowel finished on site. The top surface was sloped to allow water to drain away from the 6 inch diameter metal cap.

5.0 RELATIVE FLOOR ELEVATION SURVEYS AND CONTOURS

Mr. Robert Raffle, P.E. and Ms. Laurie Steves, E.I.T. with RKCI performed a relative floor elevation survey of the 1st floor units and the Community Center in the apartment complex. The relative elevation survey measuring equipment was placed at various locations on the interior floor surface. The relative floor elevation values were measured to the nearest hundredth of a foot; however, because the potential for error during field measurements is possible, the elevations may be considered accurate within +/-1/4 inch. The elevations were tied to the permanent benchmark set in an island on the east side of the parking lot. To facilitate the relative floor elevation survey and for the purposes of this document, an arbitrary value of 100.00 inches had been assigned to the reference benchmark. All other floor elevation measurements used in producing the drawings are relative to this assigned value of 100.00 inches. (Refer to Appendix B, Drawing C 1.0 - Relative floor elevations indicated have been corrected for floor covering thicknesses.)

A comparison of the highest and lowest elevations, the difference, straight line distance between these elevations, percent slope and equivalent elevation change over five (5) feet are provided in Table 1. Also, listed for comparison is the highest and lowest elevation difference presented in the 2011 Condition Study by Accutech Consultants LLC. Considering that the accuracy of field measurements is +/- 1/4 inch (+/- 0.25 in.), there has been no appreciable overall movement except in the West Building where the variance has reduced by nearly 2 inches. It is important to note that the percent slope presented in the table below is from the highest elevation in the building to the lowest. Localized slopes may be higher.

Building	Highest Recorded Elevation (in)	Lowest Recorded Elevation (in)	Difference Between Highest and Lowest Elevation (in)	Difference Between Highest and Lowest Elevation (in) [Accutech Condition Study – 2011]	Distance Between Highest and Lowest Elevations [*]	Percent Slope (%)	Equivalent Elevation Change Over 5-ft Distance (in)
Community Center	137.32	133.48	3.84	3.72	46.4'	0.69	0.41
North Building	136.60	129.16	7.44	7.80	133.1'	0.47	0.28
East Building	135.88	129.28	6.60	6.84	149.7'	0.37	0.22
South Building	131.80	128.92	2.88	2.52	90.6'	0.26	0.16
West Building	134.2	129.64	4.56	6.48	132.3'	0.55	0.29

TABLE 1 – RELATIVE FLOOR ELEVATION DATA

Note: *Change in floor elevation between these two points does not imply a straight slope.

The floor elevations were converted to contour lines and overlain onto a floor plan of the apartment complex as depicted in Appendix B, Drawing C 1.1. These can be compared to contours developed in Accutech's 2011 Condition Study which are included as Drawing 4 in Appendix D. In general, the contours are very similar except in the Community Building where a low area has developed in the central floor area potentially due to dewatering of underground soils from the root systems of adjacent trees.

Appendix B, Drawing C 1.1 can be summarized as follows:

Community Building

- The foundation/floor slab generally slopes downward from east to the west.
- Isolated high areas occur in the SE and NE corners while a low area occurs centrally below the kitchen.

North Building

- The foundation/floor slab generally slopes downward from the middle to the perimeter.
- Isolated high areas occur in the kitchen/bedroom areas of Units 102, 103 and 132 and the north perimeter of Unit 131.
- Isolated low areas occur along the north and south perimeter of Units 132 and 133.

<u>East Building</u>

- The foundation/floor slab generally slopes downward from west to the east.
- Isolated high areas occur along the west perimeter of Units 105 and 106 and centrally in Unit 112.

South Building

- The foundation/floor slab generally slopes downward from the north to the south and west.
- Isolated high areas occur in the NE corner of Unit 115 and the kitchen area of Unit 119.

West Building

- The foundation/floor slab generally slopes downward from the north to the south.
- Isolated high areas occur along the east perimeter of Units 129 and 130, the west perimeter of Unit 130 and the central area of Unit 123.
- An isolated low area occurs centrally in Unit 126.

6.0 PLUMBING LEAK TESTING

On December 1, 2016, Bryco Plumbing Co. Inc. performed leak testing using a Ridgid plumbing camera. Weston Tietze, E.I.T. Technician with RKCI was present during the testing. The following observations were made:

- The original plumbing drawings showed the sanitary sewer lines incorrectly. The investigation charted the general location of the sanitary sewer main lines which are presented in Appendix B, Drawing C 1.4
- In Unit 107 (East Building), a break in the 4" trunk line was discovered. It was located in the shower drain just above the trunk line. Upon inspection with the plumbing camera, it was noticed that roots were growing inside the pipe.
- In Unit 128 (West Building), a break in the 4" trunk line was discovered. It was located underneath the shower area.
- In Unit 131 (North Building), a break in the 4" trunk line was discovered. It was located underneath the master closet.
- Rises and dips were discovered throughout the underground system which were too numerous to chart.

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Since major breaks in the sanitary sewer mains were discovered, static testing of the sanitary sewer was not conducted. Branch lines smaller than 4" including those extending to kitchen areas were not inspected. Similarly, hydrostatic testing of the domestic water lines was not conducted since no water lines traverse below the building foundation except at the solitary entrance to the hot water boiler room in the Community Building. Refer to Appendix C for Bryco Plumbing's report.

A. GEOLOGY

7.0 BORINGS AND LABORATORY TESTS

A review of the *Geologic Atlas of Texas, San Antonio Sheet,* indicates that this site lie between the soils/rock of the Pecan Gap Chalk and the Austin Chalk Formations.

The Austin Chalk is a form of limestone with intermittent seams of chalky marl and clay. Compared to other limestone formations in the San Antonio area such as Edwards Limestone, the Austin Chalk is comparatively softer in induration but is still considered a very hard rock substance and often contains harder, massive seams, layers, and/or ridges. The Austin Chalk also can contain karstic features in the form of open and/or clay-filled vugs, voids, and/or solution cavities that form as a result of solution movement through fractures in the rock mass.

Key geotechnical engineering considerations for development supported on this formation will be the depth to rock, the expansive nature of the overlying clays, the condition of the rock, and the presence/absence of karstic features.

The Pecan Gap Chalk weathers to form moderately deep soil and typically consists of clays, marly clays, and marl grading to chalk at depth. Thin seams of bentonite and/or bentonitic clays are also often encountered in this formation. Because such seams are typically thin and random, they are often difficult to locate and identify with standard geotechnical sampling methods and sampling intervals. Key geotechnical engineering concerns for development supported on this formation are expansive, soil-related movement, the condition of the rock, if present, and the presence/absence of karstic features.

B. SOIL BORINGS

Subsurface conditions at the site were evaluated by two exterior borings and four interior borings drilled at the locations shown on the Boring Location Map, Appendix B - Drawing C 1.3. These locations are approximate and distances were measured using a hand-held, recreational-grade GPS locator; tape; angles; pacing; etc. Ground penetrating radar was used to locate slab reinforcement and posttensioning tendons prior to boring to avoid damage. The exterior borings were drilled to depths of 30 ft below the existing ground surface using a truck-mounted drilling rig. The interior borings were drilled to a depth of 15 ft below the existing slab surface using a track mounted geoprobe rig. During drilling operations, the following samples were collected:

Type of Sample	Number Collected
Split-Spoon (with Standard Penetration Test)	13
Undisturbed Shelby Tube	62

Each sample was visually classified in the laboratory by a member of our engineering staff. The geotechnical engineering properties of the strata were evaluated by the following tests:

Type of Test	Number Conducted
Natural Moisture Content	75
Atterberg Limits	19
Pocket Pens	53
Unconfined Compression	5

Appendix B, Drawing C 1.3 presents the results of all laboratory and field tests in graphical or numerical form on the boring logs. A key to classification terms and symbols used on the logs is also depicted there.

Standard Penetration Test results are noted as "blows per ft" on the boring logs, where "blows per ft" refers to the number of blows by a falling hammer required for 1 ft of penetration into the soil/weak rock (N-value). Where hard or dense materials were encountered, the tests were terminated at 25 blows for 0 in. of penetration or 50 blows even if one foot of penetration had not been achieved. When all 50 blows fall within the first 6 in. (seating blows), refusal "ref" for 6 in. or less will be noted on the boring logs (Refer Appendix B - Drawing C 1.3).

Samples will be retained in our laboratory for 30 days after submittal of this report. Other arrangements may be provided at the request of the Client.

C. STRATIGRAPHY

The subsurface stratigraphy at this site can be described by three generalized strata. Each stratum has been designated by grouping soils that possess similar physical and engineering characteristics. The boring logs should be consulted for more specific stratigraphic information. The lines designating the interfaces between strata on the boring logs represent approximate boundaries. Transitions between strata may be gradual.

Stratum I consists of fill materials. The fill material in the interior borings consists of sand with traces of gravel. No samples of the fill material below the pavement were taken for visual classification. This stratum extends to depths of 1 ft below the existing pavement/slab surface in our borings.

Stratum II consists of firm to hard dark brown clay with calcareous deposits. These soils are classified as plastic to highly plastic with measured plasticity indices ranging from 31 to 50. Measured moisture contents range from 14 to 24 percent. Standard Penetration Test (SPT) N-values range from 8 to 21 blows per ft. Undrained cohesion ranges from 1.95 to 2.77 tsf based on unconfined compression test data. Undrained cohesion ranges from 2.13 to 2.25 based on pocket pen test data. Unit dry weight ranges from 105 to 118 pcf. This stratum extends to depths ranging from 2-1/2 to 9 ft below the existing ground surface in our borings.

Stratum III consists of stiff to hard tan clay. These soils are classified as plastic to highly plastic with measured plasticity indices ranging from 27 to 42. Measured moisture contents range from 8 to 21 percent. Standard Penetration Test (SPT) N-values range from 17 to 28 blows per ft. Undrained cohesion ranges from 4.55 to 4.74 tsf based on unconfined compression test data. Undrained cohesion

is 2.25 tsf based on pocket pen test data. Unit dry weight ranges from 121 to 125 pcf. All borings terminate in this stratum.

D. GROUNDWATER

Groundwater was not observed in the borings either during or immediately upon completion of the drilling operations. All borings remained dry during the field exploration phase. However, it is possible for groundwater to exist beneath this site at shallow depths on a transient basis. Fluctuations in groundwater levels occur due to variation in rainfall and surface water run-off.

E. EXPANSIVE SOIL-RELATED MOVEMENTS

The anticipated ground movements due to swelling of the underlying soils at the site were estimated for slab-on-grade construction using the empirical procedure, Texas Department of Transportation (TxDOT) Tex-124-E, Method for Determining the Potential Vertical Rise (PVR). PVR values ranging from 2-1/2 to 4-1/2 in. were estimated for the stratigraphic conditions encountered in our borings. A surcharge load of 1 psi (concrete slab and sand layer), an active zone of 15 ft, and dry moisture conditions were assumed in estimating the above PVR values.

The TxDOT method of estimating expansive soil-related movements is based on empirical correlations utilizing the measured plasticity indices and assuming typical seasonal fluctuations in moisture content. If desired, other methods of estimating expansive soil-related movements are available, such as estimations based on swell tests and/or soil-suction analyses. However, the performance of these tests and the detailed analysis of expansive soil-related movements were beyond the scope of the current study. It should also be noted that actual movements can exceed the calculated PVR values due to isolated changes in moisture content (such as due to leaks, landscape watering....) or if water seeps into the soils to greater depths than the assumed active zone depth due to deep trenching or excavations.

F. CHARACTERISTICS OF EXPANSIVE SOILS

The clay soils encountered in the borings are considered to be expansive to highly expansive soils. Expansive soils are clay soils that exhibit volume changes with changes in soil water content. Expansive soils shrink or reduce their volume when they desiccate (damp to dry) and swell or increase their volume when they gain water (moist to wet).

Expansive soils are often identified by the Atterberg Limits laboratory test. The Atterberg Limits test provides two soil parameters, Liquid Limit and Plastic Limit. The Liquid Limit is the water content of the soil mass at which clay begins to act as a viscous liquid. The Plastic Limit is the water content of the soil mass at which a clay soil begins to break apart and loses its ability to deform without breaking into pieces. The numerical difference between the Liquid Limit and Plastic Limit is known as the Plasticity Index. Generally, the shrink/swell potential of a clay soil increases as the Plasticity Index increases. Therefore, clay soils with relatively large Plasticity Indices generally exhibit greater shrink/swell behavior than clay soils with relatively small Plasticity Indices.

Since the shrinking and swelling behavior of the clay soils depends on changes in soil moisture, satisfactory long-term performance of a foundation is affected by conditions that can affect soil water content. Such conditions may include climate, vegetation, plumbing leaks, irrigation, and site drainage. Semi-arid climates (climates where periods of rainfall are followed by extended periods without rainfall)

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are more susceptible to shrink/swell behavior than climates that tend to remain either wet or dry/desiccated.

In addition, the type and extent of vegetation affects the water content of the soil since some types of trees, shrubs, and grasses require more moisture than others. The extent to which the vegetation is watered (or not watered) also directly affects soil moisture conditions, as do the surface drainage conditions around a foundation. These conditions are prevalent at this site where mature trees and shrubs were observed adjacent to the building.

G. FACTORS THAT MAY CONTRIBUTE TO DIFFERENTIAL FOUNDATION MOVEMENT

There are several factors that may contribute to differential movement of slab-on grade foundations. Some of those factors include the presence of fill soil and the condition of its placement, volumetric changes of expansive soils, vegetation effects, variations in climatic conditions, and poor surface drainage. The degree with which these factors impact the performance of the foundations and the manner in which the foundations deflect depends greatly upon their stiffness, which is a factor of design and construction practices.

Typically, when expansive soils dry from a moistened state, the soil volume decreases (shrink). Downward movement of a foundation can occur due to decreasing support for the foundation due to soil shrinkage. Soil water content beneath an existing foundation can decrease due to drying/desiccating of the surficial soil around the foundation and vegetation removing water via root systems. Cyclical wetting and drying/desiccating of the soils that support a foundation can cause recurrent differential foundation movement.

Conversely, when moisture is introduced into these soils, the soil volume increases (swell). These swell pressures can cause upward movement of a foundation. There are many possible moisture sources that can potentially increase the water content of clay soils below a foundation such as plumbing leaks, poor surface drainage, extensive landscape watering, and roof runoff discharge to name a few. This is particularly true of this site where plumbing leaks have occurred, mature trees are in close proximity to the foundations, and the downspouts empty into the planter beds or in close proximity to the foundations.

8.0 TEST PIT OBSERVATIONS

Two test pits were dug by GeoTest at the site under the observation of Robert Raffle, P.E. from RKCI. Test Pit 1 was located directly below the southern building expansion joint of the West Building and Test Pit 2 was located directly below the southern building expansion joint of the East Building. Reference is made to Appendix A, Photos 68 ad 69, respectively and Appendix B - Drawing C 1.2. Cracks in the perimeter foundation beams were noted to extend through the members but there was no differential movement on either side of the cracks. The concrete foundation beams and the portion of drilled piers that were visible appeared solid with no deterioration, spalling or exposed reinforcement. The drilled pier at Test Pit 1 was just north of the beam crack while the drilled pier at Test Pit 2 was directly below the beam crack.

9.0 CONCLUSIONS AND RECOMMENDATIONS

A. FOUNDATIONS

The ground supported beam and slab foundations of the apartment complex buildings have been adversely affected by expansive, soil related movements resulting from the condition of the fill materials, plumbing leaks, poor drainage conditions, and vegetation. The active soil zone in the San Antonio area is known to vary from about 15 to 20 feet below ground surface and is described as the zone of soil in which the moisture content in the soils varies with changes in the climate.

Although an aggressive approach to mitigating the foundation movements by adding more drilled piers or underpinning could be undertaken, it is RKCI's opinion that remedying the causes affecting soil moisture conditions be implemented first followed by a re-evaluation using floor elevation monitoring. We believe this to be the more cost effective approach for the following reasons:

- Although proper design and installation of underpinning piers can beneficially "level" and provide support for grade beams subjected to subgrade settlement and/or shrinkage, underpinning piers does not counteract subgrade heave conditions.
- By addressing the primary causes of soil moisture changes and allowing the foundations to stabilize, we get a better picture of where underpinning can be beneficial.
- Underpinning the foundation may cause further damage to the existing sanitary sewer and domestic water lines.
- In difference to other SAHA apartment complexes experiencing significant building distress due to foundation movements, it is important to reiterate that ninety-one (91) short concrete piers were installed originally and eighty-seven (87) steel piers were added in 1989 and that the floor elevation patterns measured in 2011 are not appreciably different to those presented in this report.

B. ENVIRONMENTAL CONDITIONS

The first priorities should be to remove the large trees and shrubs in close proximity to the building foundations both along the apartment building perimeters and within the courtyard and remedy the poor or improper drainage conditions that exist along the North and West Buildings by providing positive drainage away the building perimeters by either regrading, resloping existing rainwater conductors and/or adding new conductors/trenches.

C. PLUMBING SYSTEMS

Following a period of 6 to 12 months after all environmental conditions have been rectified, the underground sanitary sewer main breaks need to be repaired but, more importantly, the rises and dips observed during the leak testing must be eliminated also. RKCI recommends abandoning the existing sanitary sewer mains that run under the buildings and replumb the apartment units to direct effluent flow to the rear of each apartment tying into new sanitary sewer mains located along the exterior periphery of the apartment complex. New tie-ins would be detailed with flexible connections to mitigate effects of soil movements.

D. ROOF SYSTEMS & BUILDING EXPANSION JOINTS

The roof systems are generally in poor condition. After the recommendations under plumbing systems are complete and following a stabilization period of 6 to 12 months, RKCI recommends complete roof replacement or major roof and flashing repairs.

In conjunction with roof replacement/repair, the building expansion joints located in the exterior walls, building roofs and canopy roofs need to be replaced.

E. GENERAL REPAIRS AND MONITORING

Crack repairs were evidenced throughout the apartment complex in various interior and exterior assemblies. These repairs will need to continue as required; however, their extent and severity should diminish as major repairs recommended above are completed. Of immediate importance will be the replacement of sheathing, stucco veneer and related insulation and flashing at the 3rd floor walkway canopy facades between the North and East Building and the North and West Building (Refer to Appendix A, Photos 70, 71, 83 and 94).

Floor elevation monitoring on an annual basis for a period of five (5) years should be undertaken to evaluate the effectiveness of major environmental, plumbing, roof and building expansion joint repairs.

10.0 LIMITATIONS

The information provided in this document was prepared for the San Antonio Housing Authority (Client), and may not contain sufficient information for others and/or for other uses. The comments, opinions, and recommendations submitted in this report are based on our visual observations, the field data collected as part of the floor slope measurements and non-destructive testing, and our understanding of the project information provided to us by others. Not all distress conditions throughout the building were documented; however, general representations of the observed conditions are discussed in this document. Additional conditions may exist or may have existed at the time of our observations. If the information described in this document that was provided by others is incorrect, or if additional information becomes available, RKCI may need to revise the opinions and recommendations presented herein.

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APPENDIX A

Photo Exhibits







Photo 1 – Walkway Cracks near Unit 113



Photo 2 – Walkway Cracks near SE Community Exit



Photo 3 – Unit 114: Wall Cracks near Closet



Photo 4 – Unit 113: South Wall Crack in Living Room





Photo 5 – Unit 113: Cracks at Kitchen Counter



Photo 6 – Unit 113: Cracks at Kitchen Counter



Photo 7 – Unit 113: Cracks above doors in Hallway



Photo 8 – Unit 113: Crack in NE corner of Bedroom





Photo 9 – Unit 113: Cracks Shower Corner



Photo 10 – Unit 112: Heaving of Floor near Kitchen



Photo 11 – Unit 112: Crack in SE Corner of Living Room



Photo 12 – Unit 112: Crack near Kitchen Counter





Photo 13 – Unit 112: Cracks in Bathroom



Photo 14 – Unit 112: Cracks near Bedroom Closet



Photo 15 – Unit 111: Crack near Kitchen Counter





Photo 16 – Unit 111: Heaving and Crack in Kitchen Floor



Photo 17 – Unit 108: Wall Crack in Living Room



Photo 18 – Walkway Crack near Unit 107





Photo 19 – Unit 105: Crack in Living Room near Closet



Photo 20 – Walkway Crack near NE Community Exit



Photo 21 – Unit 103: Crack in Living Room



Photo 22 – Walkway Crack near Unit 102



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Photo 23 – Unit 134: Crack in Living Room



Photo 24 – Walkway Ceiling Crack near Unit 132



Photo 25 – Unit 131: Crack in NE Corner of Bedroom



Photo 26 – Walkway Crack near NW Community Exit





Photo 27 – Unit 129: Crack in SW Corner of Bedroom



Photo 28 – Unit 127: Crack in NW Corner of Bathroom



Photo 29 – 2nd Floor: Walkway Crack





Photo 30 – 2nd Floor: Walkway Ceiling Crack



Photo 31 – 2nd Floor: Walkway Crack



Photo 32 – 2nd Floor: Walkway Crack



Photo 33 – 2nd Floor: Walkway Crack





Photo 34 – 2nd Floor: Wall Crack near Elevator Lobby



Photo 35 – 2nd Floor: Cracking at Door Frame near Elevator Lobby



Photo 36 – 2nd Floor: Walkway Crack



Photo 37 – 2nd Floor: Walkway Crack





Photo 38 – 3rd Floor: Walkway Crack



Photo 39 – 3rd Floor: Walkway Crack



Photo 40 – 3rd Floor: Walkway Crack



Photo 41 – 3rd Floor: Walkway Crack





Photo 42 – 3rd Floor: Walkway Crack



Photo 43 – 3rd Floor: Walkway Crack



Photo 44 – 3rd Floor: Crack at Door Frame near Elevator Lobby



Photo 45 – 3rd Floor: Walkway Crack





Photo 47 – West Building: Deteriorated North Expansion Joint



Photo 48 – West Building: Deteriorated North Expansion Joint at Base



Photo 46 – 3rd Floor: Walkway Crack





Photo 49 – West Building: Deteriorated South Expansion Joint



Photo 50 – West Building: Deteriorated South Expansion Joint at Base



Photo 51 – West Building Foundation Crack




Photo 52 – West Building: Improper Drainage (Looking South)



Photo 53 – West Building: Improper Drainage (Looking North)



Photo 54 – West Building: South Façade Joint Separation



Photo 55 – South Building: East Façade Joint Separation





Photo 56 – East Building: Deteriorated South Expansion Joint



Photo 58 - East Building: Deteriorated North Expansion Joint



Photo 57 – East Building: Deteriorated South Expansion Joint at Base



Photo 59 - East Building: Deteriorated North Expansion Joint at Base





Photo 60 – East Building: North Facade



Photo 61 – North Building: East Façade with Crack below Window



Photo 62 –North Parking Lot: Deteriorated Concrete Joints





Photo 65 – North Building: North Façade Window Area with Vertical Crack and Sheetmetal Dam at Base



Photo 63 – North Parking Lot: Deteriorated Concrete Joints



Photo 64 –North Parking Lot: Deteriorated Concrete Joints





Photo 66 – North Building: Improper Drainage back towards Building (Looking West)



Photo 67 – North Building: Improper Drainage at NW Corner



Photo 68 –West Building: Test Pit 1





Photo 69 – East Building: Test Pit 2



Photo 70 – 3rd Floor Deteriorated Walkway Canopy Façade between North and East Buildings



Photo 71 – 3rd Floor Deteriorated Walkway Canopy Façade between North and West Buildings



Photo 72 – West Building Roof showing Hail Damage (Looking West)





Photo 73 – North Building: Walkway Canopy Roof showing Improper Patching (Looking West)



Photo 74 – East Building: North Stairway Roof showing Hail Damage



Photo 75 – East Building: Northern Roof Expansion Joint Improperly Covered with a Shingle Patch



Photo 76 – East Building Roof showing Deteriorated Vents, Penetrations, and Flashings (Looking South)





Photo 77 – East Building: Northern Deteriorated Expansion Joint at Walkway Canopy Roof



Photo 78 – East Building Southern Roof Expansion Joint Improperly Covered with a Shingle Patch



Photo 79 – East Building: Southern Deteriorated Expansion Joint at Walkway Canopy Roof



Photo 80 – East Building: Deteriorated Flashing and Roofing at Vent Penetrations





Photo 81 – South Building Roof showing Deteriorated Vents, Penetrations, and Flashings (Looking West)



Photo 83 – Walkway Canopy Connector between North and West Buildings showing Deteriorated Conditions



Photo 82 – South Building Walkway Canopy Roof showing Hail Damage and deteriorated Ridge Construction (Looking West)



Photo 84 – North Building: Walkway Canopy Roof (Looking East)





Photo 85 – North Building Roof: West End showing Facade Cracks



Photo 86 – West Building Roof showing Hail Damage (Looking North)



Photo 87 – West Building: Southern Stairway Canopy Roof showing hail Damage (Looking East)



Photo 88 – South Building: Walkway Canopy Roof (Looking East)





Photo 89 – West Building showing Deteriorated Northern Roof Expansion Joint



Photo 91 – West Building: Northern Deteriorated Expansion Joint at Walkway Canopy Roof



Photo 90 – West Building Southern Roof Expansion Joint Improperly Covered with a Shingle Patch



Photo 92 – West Building: Southern Deteriorated Expansion Joint at Walkway Canopy Roof





Photo 93 – West Building: Deteriorated Ridge Flashing and Canopy Roof (Looking South)



Photo 95 – Community Building Roof (Looking West)



Photo 94 – Walkway Canopy Connector between North and East Buildings showing Deteriorated Conditions



Photo 96 – North Building: East End showing Deteriorated Ridge and Rake Flashing and Facade Cracks (Looking North)





Photo 97 – North Building: Deteriorated Ridge and Rake Flashing



APPENDIX B

Drawing Exhibits







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PROJECT NO. ASR36-034-0

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NOTE: SANITARY SEWER DEPICTS AS-BUILT AND EXISTING CONDITIONS AS DETERMINED FROM CAMERA OBSERVATIONS CONDUCTED BY BRYCO PLUMBING CO. INC. ON DECEMBER 1, 2016.



	R	RABA KISTNER
co	Raba I 128 San	Kistner Consultants, Inc. 321 West Golden Lane Antonio, Texas 78249 www.rkci.com P 210 :: 699 :: 9090 F 210 :: 699 :: 6426 TBPE Firm F-3257
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APPENDIX C

Plumbing Leak Test Report



Bryco Plumbing Company, Inc. 14117 Toepperwein San Antonio, TX 78233



Professional Plumbing Services Licensed, Bonded, Insured 655-2552 (Fax 655-2514)

December 7, 2016

Raba Kistner Consultants 12821 W. Golden Lane San Antonio, Texas 78249

To: Robert Raffle Re: Pecan Hill 1600 W. Lawndale San Antonio, TX 78209

Bryco Plumbing Co conducted a visual inspection of the drain lines under the buildings at the above address. There were three visible breaks found under the buildings. The first break was found under unit 107 under the shower drain. The second break was found under unit 130 under the shower drain. The third leak was found under unit 131 below the master closet on the main drain. Please note: The drain lines are PVC pipe under the slab.

Please feel free to contact me with any questions you may have regarding the work that was done.

Thank you,

u7

Shawn Roberts

SAR/1bn



APPENDIX D

Foundation Elevations 2011













APAR	TMENT	PANEL	SCHEDULE										
			VOL TAOE	TYDE	C,	/B	C,	/ B	C,	/8	C,	/ B	FEEDER-(USE THW ALUMINUM)
QUANTITY	QUANTITY TYPE SIZE	VULTAGE	1175	125/3P	WIRE	50/2P	WIRE*	30/2P	WIRE	20/1F	WIRE*	S,E,U. SERVICE	
18	Å	100A.M.L.O.	120/208 V. 10	FLUSH			1	#6	1 *	#10	8	#12	3*2
69	В	100A. M.L.O.	120/208 V.10	FLUSH			- Karana	#6	1 2	#10 2	8	#12	3#2
9	Ċ	100A. M.L.O.	120/208 1.10	FLUSH	÷.		175-1	#6	1 10	#10	8	#12	3*2
4	P	100 A M.L.O.	120/208 1.10	FLUSH			1	#6	1 👘	#10	8	#12	3*2
- X	M	125A. M.L.O.	120/208 V30	SURFACE		4 10 ⁰⁰			1*	#10	1	#12	4.#2, 1-#66. 17 PVC
		125 A. M.L.O.	120 208 130	FLUSH	1	#2	2	#4			5	#12	3#2
	LZ	70 A. M.L.O.	120/208410	FLUSH		-	3 4		- s.		7	#12	3*2
$1 \frac{1}{1}$	LS	70 A.M.L.O.	120/208V.10	FLUSH			1		1	#10	10	# 2	3#4
						÷,		alle y .					

	MAIN	MLO	-	C/	/B	C,	/8	C/	/B	<u>c/</u>	· B	<u>C/</u>	8	FEEDER - (USE THW ALUMINUM)
PANEL	SOURCE	MIN.	FEEDS	500/3P	WIRE	400/3P	WIRE	225/3 P	WIRE	100/2P	WIRE	20/1 P	WIRE	PVC SERVICE UNDERGROUND
MDP	TRANSF.	1200A.	DP1,2,3,4,5	2	2-5001	Э	#500M		#350M		an an the second se			1200 AMP 120/208 V. 30 4-WIRE
PP-1 *	MDP	500	DP-IA, M 34,128 APTS.		- - -		# 300M	100,57	#2	:15	#2 ,	6	#12	3-# 500MCM, 1-#350MCM NEUT., #1/06., 2-3'2" PVC.
P-IA #	DP-1	400	GAJEB APTS		a tu					18	#2	2	#/2	3 # 250 MCM, /- "3/0 NEUT," //06. 2-22
DP-7_ #	MDP	500	DP-2A,3A,R.B				94 - 14 - 14 - 14 - 14 - 14 - 14 - 14 -		300M	15	#2	4		2 #2 ED MOM 1 - #2 CD MCM NEUT 1-#2 G
DP-ZAT	DP-2	225	68,3C12D			and a special sector of the se					#2	4	#12	2 # 350 MCM. 1-# 250 MCM NEUT 1-#26
DP-3	MDP	225	6B, 3C, 20							11	and a second		1.7	2 # CANMON 1- TASK MCM NEUT, 1-#106.
DP-4 *	MOP	400	3A, 70, 20				95 - 14 14			in	#2	7	#12	2 # 500 MCM 1-#350 MCM NEUT. 1-#10 G
)P-5 *	MDP	400	SAJILE	10-150	-into	LA /2 E	- March	50/0	41	2012P	=	29	#/2	2 # 500 MCM . 1- #350 MCM NEUT 1- #1/0 G
P-CBT	MDP	400.4		145/57	The second	3	· • • • • •	10/21		5-1-1	T 70		and the second second	
LI	DP-CB	125	L2,L3	SEE	ABO	VE								
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COPPER

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bedroom

kit.¢

living

* PANELS DP-1,2,3,4,5,08,14,24 SHALL HAVE CIRCUIT BREAKERS AS SCHEDULED AND ON LOAD SIDE OF APARTMENT BREAKERS THEY SHALL HAVE 100 A. METER SOCKETS FOR INSTALLATION OF WATTHOUR METERS FOR CONSUMPTION CHECKING BY OWNER.



UNIT-A -ELECTRICAL







UNIT-B - ELECTRICAL

dining

UNIT-C - ELECTRICAL HANDICAPPED

T.V. ANTENNA SYSTEM

INSTALL A TV ANTENNA RECEPTACLE IN EACH LIVING ROOM AS SHOWN, COMPLETE WITH BOX & PLATE. INSTALL COAXIAL CABLE FROMEACH OUTLET TO AMPLIFIER IN COMMUNITY CENTER BLDG., COMPLETE WITH SPLITTERS, CONNECTORS, TERMINAL CABINETS, ETC. CABLES SHALL BE RUN IN WALLS OR FLOOP JOIST SPACE (NO CONDUIT) AND DIRECT BURIAL (18"MIN.) OUTSIDE BLDG. INSTALL ALL BAND ANTENNA ON 3RD FLOOR ROOF. GROUND TO COLD WATER PIPE. INSTALL AMPLIFIER TO PROVIDE SUFFICIENT SIGNAL AT EACH OUTLET ON ALL LOCAL CHANNELS, WITH NO OBJECTIONABLE GHOSTS.

MANUAL FIRE ALARM SYSTEM - SEE SPECS.

bedroom bedroom PANEL "0" HOODdining

living

UNIT-D - ELECTRICAL

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TÊXAS





BUILDING PLAN - ELECTRICAL





SCALE : 1/2=1-01



SCALE: 1/4" = 1'-0"



UNIT-A MECHANICAL



HANDICAPPED







MEC	HANICAL SYMBOLS
	SUPPLY REGISTER (REG.)
]++<	RETURN GRILL (R.A.G.)
\bowtie	SUPPLY DUCT UP
= 16×6	VIEWED DIMENSION × DEPTH
	SPLITTER DAMPER
Φ	THERMOSTAT
D.G.	DOOR GRILL



PL. UNITS. 6"+ F.T.R.











UNIT-D MECHANICAL





HANDICAPPED





















BUILDING PLAN - SECOND & THIRD FL - PLBG.

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MAINTENANCE PUILDING

BY CONTRI BACKFLOW PREVENTION DEVISE IN. VALUT. (SEE DETAIL.) BY C.W.B. - 2. WATER METER IN CAST IRON VALUT

GAS SERVICE FROM MAIN THRU GAS METER FREG STATION AS DIRECTED BY C.P.S.D. BOLATION FITTINGS FACH SIDE OF LOOP.







R	DOM FINIS	H SC	HEDUL	E	
	U	NITS			r
room	floor	base	walls	celli hqt.	ng mtl.
LIVING	GARPET	WARD	OYP.BO.	8.0	GYP. BC
DINING	GARPET	HADD	BYP. BR	0.0"	BY? OC
KITCHEN	VINYL ASE TILE	SHOE MOULD	GTP. 00	0-0"	GYP. B
BEDRIOMS	CARPET	WID	GYP. OD	8.0"	619. 22
CATHER .			BYP. BQ.	7-0"8-0"	STP EC
GLOGETS & LINEN	GARPET	WOD	GYP. DD.	7-0%-0	619. BC
STORADE UNITED	CARPET VINYL AGE THE	WOOD	err da	10/8.0	GYP. BC
HALLS	CARPET	WOOD	GYP. BD.	7-01	GYP. BL
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MAINT MULTION	EXPOSED CONG	WOOD	61P. 00.	EN	6 11 pm
PLOG. COMO MATL.	EXPOSED CONC.	ZNOOD	GYP BQ	ં મ	<u>en 1</u> 1 r.
ELEV EQUIP	EXPORED CONC	WOOD-	GYP. BD.	11	ų
ZOMM. RM. MD.	EXPOSED CONG.	WOOD	GYP. BD.	8"-0"	GTPB

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		SCHEDULE	C
00		description	detail
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		SOLD CORE	n en et andere en et an en ante ante ante ante ante a
2	3-0"×0-0 × 1/8	BCREEN DOOR	IINDER ALT BR
3	3.0 × 6-0 × 1%	HOLLOW GORE	CRS FOR RIA
4	2-0 × 0-0 × 170	HOLLOW CORE	DRS FOR RIA
5	2-0 × 6-8 × 138	HOLLOW GORE	
6	1-8 × 6-8 × 13/8	HOLLOW GORE	
7	1-8" x 5-4" x 19/8"	HOLLOW CORE	
8	3-0" x 7 -0' R.O.	FOLDING DOOR	
9	4-4" x 7 -0" R.O.	ji - 1	
10	5-0" × 8-0" R.O.	ļį ļ	
- 11	-1.0" x-1-0 RO	1 1	
12	7:8" x7'-0" R.O.		
13	8.4 × 8.0 R.O.		
14	OM TED		α τη τι δια τη
15	PR-8:0'16-8" × 13/4"	BOLIC CORE	2-24,30 2EG. EACH DOOR
16	FR-2-6"x 6-8" x 19/8"	HOLLOW CORE	
17	PR-3-0" 16-8" x 13/4"	6040 CAZE	
18	2-0"×6-3"× 134"	SC. FRENCH DR.	·······
. 19	4-2" × 7'-0" 12.0.	POLDING DOOR	***
20	3-0" x7'-0" x 134"	HARROW STILLE	
21	17-4"×8'-0"	FOLDING ROOR	
22	7-11"x8'-0"	1) j	
23	A-4"×8-0"		201 M M
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SECOND FLOOR FRAMING PLAN



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BUILDING PLAN - FIRST FLOOR

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	GENERAL NO)TES: CONCRETE: MINIM	IUM COMPRESSIVE (STRENGTH OF (3000 PSI AT 28	8 DAYS.			
	2. 3.	STEEL: ALL REIN OPENINGS THROUGH OF TUB TRAP OPEN	FORCING BARS SHA SLAB: NONE LAF	ALL BE ASTM- RGER THAN 8" FILLED WITH	615 GRADE 60. WITH THE EXCE	EPTION			
	4. 5. 6.	WATERPROOFING ME 6" SELECT MATERI ALL EXTERIOR BEA	MBRANE: 6 MIL. AL CUSHION UNDEF MS SHALL BE MIN	POLYETHYLEN R SLAB WITH IMUM 6" INTO	E. P.I. LESS THAN UNDISTURBED S	N 12. SOIL.			
	7.	ALL OTHER BEAMS HAS BEEN COMPACT ACCORDANCE WITH	6" INTO UNDISTUR ED TO NOT LESS 1 ASTM DENSITY TES	RBED SOIL UN THAN 90% OF ∣ ST NO. D 155	LESS FILL UNDE MAXIMUM DENSI1 7-58T OR 95% (ER SLAB TY IN DF THE			
		MAXIMUM DENSITY TEST (ASTM D 155 LOOSE LIFTS NOT	IN ACCORDANCE WI 7-70). THE FILL EXCEEDING 8" IN	ITH MODIFIED _ MATERIAL S THICKNESS.	PROCTOR COMPA HOULD BE PLACE	ACTION ED IN			
	8 .	WHERE CALLED FOR STRAND 3/8" IN D WITH A PLASTIC S	, ALL TENDONS SH IAMETER OR 1/2" LEEVE.	ALL BE 270 IN DIAMETER	K GRADE 7 WIRE , GREASED AND	E STEEL Sheathed			
	9. 10.	ANCHORS FOR THE AND SHALL CONFOR ALL 3/8" TENDONS	TENDONS SHALL BE M TO ACI REQUIRE SHALL BE POST-1	E MANUFACTUR EMENTS. TENSIONED TO	ED BY RELIABLE	E ELECTRIC			
		18,500 POUNDS EA 33,000 POUNDS EA DIRECTED BY THE	CH AND ALL 1/2" CH. THE POST-TE ENGINEER AND SH/	TENDONS TO ENSIONING SH ALL <u>NOT</u> BE A	AN INITIAL STR ALL BE APPLIED PPLIED UNTIL 1	RESS_OF D_AS The_CON-			
	11.	CRETE HAS ATTAIN UNLESS APPROVED ALL BARS AND/OR	ED A MINIMUM COM OTHERWISE. TENDONS ARE TO E	1PRESSIVE ST	RENGTH OF 2000) PSI, AND SLAB			
		WITH CHAIRS OR S INTERSECTION IN TENDONS.	LAB BOLSTERS, AN CASE OF BARS AND	ID SHALL BE	TIED AT EVERY RSECTION IN CA	OTHER ASE OF		and the second	
	12.	CABLES OVER 75' CONTRACTOR TO VE LOCATIONS WITH A	IN LENGTH SHALL RIFY ALL DIMENSI RCHITECT'S FLOOF	HAVE "LIVE" (ONS, DROP A R PLAN.	ENDS AT BUTH REAS AND BLOCK	ENDS. COUT			
	14.	WITHIN 15 FEET O PROVIDE POSITIVE	F SLAB PERIMETER DRAINAGE AWAY F	TROM THE SLA	B PERIMETER.				
		THE SURROUNDING (SLOPED DOWN AND)	AVAY FROM THE EE	D BE A MINI GRADE. TH DGE OF THE S	E GROUND SHOUL AB FOR 25 FEE	LD BE ET AT A			
	WE, MAVERI	2% SLOPE. CK ENGINEERING CO	OMPANY, CERTIFY	THAT THIS FO	OUNDATIONSLA	AB AND ITS		a an a than an a An an	
	FOR THE SO	T REAR DEDOUT OF	DETERMINED BY S	OIL ANALYSIS	S PREPARED BY	1973 F REEN LICEN			
	IN ESTABLE	SHING THE DESIGN	REQUIREMENTS FO	R THIS FOUND	DATION.	L DELN USEU			
	SOIL CLASS	IFICATION CH	<u> </u>	BUILDER		 2ANY			
				BY: Jativ	A. DI	esa'			
		DATE <u>/-28</u>	- 7.3	JOB NO	5-102 6	45			
	1. (1999) 1. (1999) 1. (1999) 1. (1999) 1. (1999)			С. 222 г. Г					
e e e e e e e e e e e e e e e e e e e			Xe						
			MALAN CON		MAVERIC ENGINEER	UNG			
and gains	Sec. 3		A-ANA CONST	89997 The 46855			10400 2009		
						.5			

tree staking details

tree planting detail

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4	SENERAL NOTES		tree and
1	. TREE & SHRUB LOCATIONS ARE APPROX. ON THIS PLAN.	key	common name
	ARCHIEL ON SIE DEERMINE EART LOCATOR	GC1	COTTONLESS COTTONINO
	2. MAINTAIN MIN. 4 CLEARANCE BETWEEN GHRIDE & BLOGS.	9	STCAMORE
-	- LANGERING LAND - LEADANCE	J.P.	JAPANESE FLUM
	2 MAIN AIN MIN. A CLEARANCE DEIWEEN INDE & DUCOS-	P	PITTOSPORUM VARIESAT
	F. GOLID GOD TO ELGE ALL WALKS, UKIVES & CURDS WI 12" WIDE MATS	C.M.	CRAPE MYRTLE MULTI-
1	3. GOLD GOD ALL GLOPEG GREATER THAN 2 HORIZ. IVENT.	PTT.GR.	PITTOSPORUM GREEN
4	5 GOLID GOD DRAINAGE GWALED	BOX	JAPANESE BOXWOOD
•	7. SOLID SOD & GPRINGEREMAINDER DE BROUNDE AS NOTED	PHOT.	PHOTINIA
	a courto an allow and the charge legation poor shing & Allowen to	WAX LF	WALEAF LIGUSTRUM
4	SETTLE BY WATERING PROCESS CONTINUED UNTIL TREE WELL IS FILLED		ST. AUGUSTINE
	WEDIL TO LEVEL AS SHOWN IN DETAIL	H.F.	HOUT FERN
ć	1, SOIL ACIDIFIER TO BE "GREEN LIGHT" SOIL ACIDIFIER.	EHG.	EHGLIGH MY
	O SHRUDS IN NOWS TO BE FLANIED IN INENCHOS & DEEF & B WIPE		
	I ALL GRAGS TO BE WATERED DAILY FOR INT TWO WEEKS AFTER FLANTING.		
	2. ALL TREE WELLS TO BE FILLED WITH A HIGH QUALITY LOAM SOLL FREE OF		
	HEROKIVES, FEIGURES, EK.	······································	
1	3. ALL PLANT MATERIAL GHALL COMPLY WI THE SPECIFICATIONS OUTLINED IN THE HILD - FHA HANDROOK, DET-41423, DATA SHEET SO-101		
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PART			
M			
FER			
- F		LEGE	
		(22) 1	NEW TREE
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		- <i>(())</i> > #	EXECTING TREE TO
			EXISTING THE TO B
			nne om distant. Heading in her is

and	shrub schedule		
me	scientific name	qnty	size and remarks
ONMOOD	BPULAI CANDICANS	a	12"CALIP 3-10' B.B.
	PLATANUS OCCIDENTALIS	1	1/2" CALIP 8-10' BB.
M	LASUAT		GAL. 18"
LESATED	PITTOS BRUM TOBIRA, VARIEGATE		16AL 12"-18"
TULTI - BR	WHI LASERSTROEMA MULTI-TRUNK		5GAL. 30"-36"
EN.	PITROSPORUM TOBIRA, GREEN		16AL. 12"-18"
NOOD	BUXUS MICROPHYLA JARONICA		1GAL. 12"
	PHOTINIA FRAGERI		GAL. 2"-18"
TRUM	LIGUSTRUM, TEXANA		B&B B"-24"
2	STENDTAPHRUM SECUNDATUM		5010 200 OR SPREGING ASS
	CTRIDMIUM FALCATUM		
	Hedera Helix		
		_	
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TO REMAIN

TO BE REMOVED

ÌĎ ----MAINT. BLDG. PHOT 6 æ 21/11 _____ 0 -2-WAX ------ J P. -50110 VEGETABLE GARDENS OTIT STRIGS N WAX LF WAX L.F. -----A WALF. ----------Ø REGINO ATTOR .

landscape plan

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SECTION

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	CURVE DATA								
CURVE	DELTA	RADIUS	TANGENT	LENG1					
A	180°00'00"	4.08'		12.32					
в	154°22'41"	6.00'	26.39'	16.17					
C	64° 22' 41*	31.00'	19.51'	34.83					
D	90°00'00"	5.00'	5.00'	7.85'					
E	90.00'00"	6.00'	6.00'	9.42'					
F	180°00'00'	3.60'	-	11.30'					
G	90°00'00*	10.00' .	10.00'	15.70					
Н	180°00'00"	4.50'		14.14					

BROWN FATTY CLAY, CH YELLOWIGH BROWN PATTY CLAY, CH YELLOW GILTY CLAY, GL YELLOW BRAY BILTY CLAY, CL. BLOCKY

YELLOW FATTY CLAY, CH WITH BEAMS BRAY BILT ; BLOCKY TO BHALBY

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RAILING ONE SIDE ONLY 142 STD FIPE, GET IN SLEEVES.

TYP CONC WALK

EUCATION

SONC CURD O

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MAIN

CONC SUB

SONC

VELLOWIGH BROWN FATTY CLAY, CH WITH TRACE CALCAREOUS MATERIAL YELLOW SILTY GLAY, EL YELLOW - GRAY BILTY CLAY, CL YELLOW FATTY GLAY, CH WITH GRANG BRAY SILTY, BLOGKY ; AT 4 TO 14.9 FT. BYPGUM CRYSTALE IN JOINTS

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WOOD FENG

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OWNE

SAN ANTONIO HOUSING AUTHORITY 100 UNIT ELDERLY PROJECT LAWNDALE DRIVE SAN ANTONIO, TEXAS HUD PROJECT NO. TEX. 59-0007-004

architect

purchaser seller

approvals

:	ralph c. bender & assoc. inc.
:	san antonio housing authority
:	title : lee – jackson – turner inc.
	title :
	san antonio hud insuring office
	tite : date :

ralph c. bender & assoc. inc.

environmental planning • urban design • architecture

8026 vantage drive san antonio

phone : 512 · 342 · 3291 texas, 78230

19 .

area legend

<u>type</u>	no. units	unit area	total
unit A	18	493	8874
unit B& B-I	69	572	39,468
unit C & C-I	9	572	5148
unit D	4	820	3280
totals	100		56,770
community bldg.	4966		
maint. bldg.	800		

topographical plan

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site plan site staking plan grading, paving and drainage plan landscape plan site engineering details foundation plan foundation plan and details building plan – first floor building plan - second floor building plan - third floor unit floor plans community building and elevator lobby plans building elevations building sections and elevations second floor framing plan roof framing plan — partial third floor framing plan roof plan and details wall sections elevator and lobby section typical stair section - maintenance building plan wall sections - door, window and room finish schedules door and window details plumbing site plan plumbing building plan – first floor plumbing building plan - second and third floor plumbing unit floor plans schematic piping details air cond. unit floor plans air cond. community bldg. lobby and maint. bldg. electrical site plan electrical building plans electrical unit floor plans electrical community building, lobby and maint. bldg.

drawing index